45

Studies into the aerodynamics of heating chambers for raw-smoked sausages and the deter-mination of hydraulic resistances of air-distribution systems

SUKHANOVA S.I., BABANOV I.G., and BRAZHNIKOV A.M.*, MINAEV A.I.** The All-Union Meat Research Institute, Moscow, USSR *The Moscow Technological Institute of Meat & Dairy Industries, Moscow, USSR "The RSFSR State Agro-Industrial Committee, Moscow, USSR

On designing equipment for raw-smoked sausages heating and drying it is necessary to calculate hydraulic (aerodynamic) resistance of a fuel mixture stream in the processing sone

taking into account physico-chemical processes. To evaluate the efficiency of a proposed pulsed fuel mixture feed to the processing zone and to determine hydraulic resistances, aerodynamics of chamber-type installation for raw-smoked sausages heat treatment is investigated.

Fuel mixture for sausage heat treatment is investigated. Fuel mixture for sausage heating equipment represents a heterogeneous binary system /1/. Heat-exchange processes in these apparatus are followed with steam condensation from moist air on product's surface or with moisture evaporation. The presented stream of a fuel mix-ture influences the character of mixture's flow in the boundary layer thus changing hydro-

mechanical conditions and heat-mass transfer/2/. From the results of investigations the average rate / \overline{u} /of fuel mixture flow in the pro-cessing zone is 0.3 m/s., critical Reynold's number (Re) - 8.0 x 10³. The fuel mixture flow regiene is laminary. At the laminer manual flow regions for the fuel mixture flow in the pro-

At the laminary regiene of the fuel mixture flow connective heat transfer coefficient(d) is determined from the following relationship/3/:

$$N_{\mu} = 0.66 \text{ Re}^{02}$$

 $d = N_{\mu} \lambda$

where: \mathcal{N}_{u} - Nusselt's criterion; \mathcal{I} - air thermal condustivity, $W/m^{2}K$; \mathcal{E} - sausage stick length, m.

 $\alpha = 3.83 \text{W/m}^2 \text{K}$

The obtained values of heat transfer coefficient (α)(from a fuel mixture to a product) should be taken into account at chamber-type installation designing with a pubsed fuel This ture feed used for raw-smoked sausages processing. Hydraulic resistances and pressure losses of the fuel mixture in the processing zone were calculated according to I.E.Ideltchik procedure /4/.

Experimental and analytical methods, traditional for applied aerodynamics and hydraulics,

Were used /5/. At calculation of total fuel mixture flow losses were taken into account. They consisted of losses at processing zone inlet and outlet and of losses due to friction. The total coefficient of resistance in the frame with products (at one-store sausage hancing) couple.

where: β_{i} - barrier's coefficient (cylinder), being determined according to a reference book /4/, $\beta_{i} = 1.76$; $K_{i} = \left(\frac{S_{i}}{a_{i}} - t\right) - according to the graph /4/, <math>K_{i} = 1$; $S_{i} - distance$ between sausage sticks' axises, m; a_{o} - distance between sausage sticks, m; a_{o} - distance between sausage sticks, m;

- a coefficient characterizing a specific form of sausage, n=1.5; - linear coefficient of friction resistance, $\Lambda = \frac{64}{Re}$;

d - sausage diameter, m. According to the formulae the total hydraulic resistance of fuel mixture equals:to:

$$\xi_{tot} = 3$$
.

Therefore, losses of the fuel mixture flow (ap) in the processing zone are: op= & Puz

where: β - air density according to the reference book /4/, β = 1.2 kg/m³.

AP = 0.162 Pa. At two-stored sausage hanging:

 $\Delta p = 0.324$ Pa. Obtained total coefficients of hydraulic resistances (5) and pressure losses (Δp) of the fuel mixture in the processing zone are not significant; they may be emmited at cham-ber-type installation designing. Fot the chambers with one-stored distribution of pro-ducts hydrodynamics of air-distribution system should be taken into account (air ducts of the fuel mixture discharge under pressure and suction). At more than one-stored frame distribution by height total coefficient of resistance (δr and pressure losses (Δp) increase and influence air distribution in the processing zone. Ap = 0.324 Pa.

References

I. Богословский В.И., Поз М.Я. Теплофизика аппаратов утилизации тепла, систем отопления, Вентиляции и кондиционирования. - М., Стройиздат, 1983, -318с. 2. Дибан Е.П., Эпик Э.Я. Тепломассообмен и гидродинамика турбулизированных потоков. -Кмев, Наука, 1985, -296с. 3. Исаченко В.П., Осипова В.А., Сукомел А.С. Теплопередача. -М., Энергия, 1981, -417с. 4. Царльчик М.Е. Справочник по гидравлическим сопротивлениям. - М., Машиностроение, 1975,

-460с. 5. Повх И.Л. Аэродинамический эксперимент в машиностроении. – Л. Машиностроение, 1974, -779с.