

THE ROLE OF VARIOUS PROCESSES IN MANUFACTURING A LOW SODIUM RESTRUCTURED HAM

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INTRODUCTION

Sodium chloride (NaCl) is an essential ingredient in processed meat products, since it can contribute to: (i) solubilization of meat proteins responsible for the binding and texture of the cooked product (ii) providing the typical salty flavour and (iii) control microbial growth. However, sodium reduction, in the Western diet, is currently recommended as a means of decreasing hypertension and subsequent cardiovascular diseases. Growing consumer demand for low salt products has resulted in extensive research aimed to reduce the sodium levels in processed meat products. Some of the ways that have been suggested to do so, without adversely affecting the quality of the meat products include: slight NaCl reduction, replacing NaCl with non-chloride salts, the use of phosphates, altering processing methods (i.e., vacuum tumbling, massaging, use of pre-rigor meat) and/or various combinations of the above.

Among the non-chloride salts potassium chloride (KCl) has been indicated as the most suitable substitute for NaCl. However, due to off-flavour problems only partial substitution with KCl is recommended (Barbut and Findlay, 1989). Phosphate addition can further reduce the amount of NaCl required (Ockerman et al., 1978). The advantages of using mechanical action basically include improvement in tenderness, increasing colour and texture uniformity, and reducing processing time (Pearson and Tauber, 1984).

This paper describes the effects of tumbling parameters and KCl substitution on the quality of reduced sodium restructured ham.

METHODS AND MATERIALS

Experimental design

A rotatable central composite design was used with three variables: (i) tumbling time (6, 8.4, 12, 15.6, and 18 hr) (X1), (ii) tumbling speed (7, 11, 17, 23 and 27 rpm) (X2), and (iii) % KCl substitution (0, 15.2, 37.5, 60 and 75) (X3). This design consisted of 6 central, 6 star and 2³-(8) factorial experiments i.e. 20 treatments. Tumbling was performed using intermittent cycling (25 min/hr). The minimum and maximum number of cumulative revolutions were 1050 and 12150, respectively. Percent KCl substitution was based on producing an equivalent ionic strength of 2% NaCl (i.e., equivalent ionic strength of 0.342).

Ham preparation

Boneless pork muscles (semi membranous, adductor, biceps femoris and semi tendinosus) were ground through a kidney plate (Hobart, Don Mills, Ontario), and pork fat was ground three times through a 3.2 cm plate. Lean pork contained 73.3% moisture, 21.5% protein, 4.2% fat and 1.1% ash; and pork fat contained 59.7% fat, 37.3% moisture, 3.1% protein and 0.1% ash. Hams (3.0 kg/treatment) were formulated to contain 10% fat. The raw meat was stored at -20°C until needed and then thawed for 2 days at 2°C.

The total mass of the curing solution in each treatment was equivalent to 15% of the total raw material. Its composition was: 0.012% sodium nitrite, 0.055% sodium erythorbate, 0.25% sodium tripolyphosphate, 0.33% sugar, 0.04% nutmeg and 0.15% black pepper. The variables were NaCl, KCl and water. The raw meat was tumbled

under vacuum (67.7 KPa) intermittently (25 min/hr) in a table-top tumbler (Lyco, model 40, Columbus, WI) at 2 C.

Cured meat was stuffed into 60 mm diameter moisture-proof casings (Teepak, Oak Brook, IL) using a hand stuffer (A.M.B., Bologna, Italy). Ham rolls were cooked in a steam jacketed kettle at 73-77°C until an internal temperature of 69-71°C was reached. Cooked ham was cooled in an ice water bath for 30 min, and stored at 2°C.

Quality measurement

Cooking yield (CY) was calculated by dividing the cooked ham mass by the uncooked ham mass. To measure shrinkage (SH), each ham roll was sliced in half to allow the draining of retained juice for 45 min. The shrinkage was computed as the ratio of the change in the ham mass before and after cooking.

A spectroguard Color System (Pacific Scientific Co., Model 96, Silver Spring, MD) was used to measure the cooked ham colour. The Hunter Color Lab scale parameters of 'L', 'a' and 'b' were measured. The centrifugal method of Bouton et al. (1971) was used to determine water holding capacity (WHC).

The Instron Universal Testing Machine (Model 4204) was used to measure the texture profile analysis (TPA) parameters (Bourne, 1978). Each sample (2 cm in dia. and 1.5 cm in height) was compressed twice to 75% of its original height. Cross head and chart speeds were 20 mm/min and 100 mm/min, respectively. TPA parameters

included hardness (HARD), cohesiveness (COH), elasticity (ELAS), gumminess (GUM) and chewiness (CHEW). Warner-Bratzler Shear (WBS) was determined by measuring the maximum force (kg) required to shear the cooked samples. Samples' dimensions were similar to the TPA.

The taste panel consisted of 12 to 20 semi-trained judges. They evaluated the colour (COL), tenderness (TEND), juiciness (JUIC), saltiness (SALT), off flavour (OF) and overall acceptability (OA) of the products. The ballot used consisted of 15 cm long horizontal lines (Stone et al., 1974) where the most desirable attribute was at the far right side. Results were obtained by measuring the distance from the left side of the scale in cm.

For statistical analysis, the Statistical Analysis System (SAS 1982) was used.

RESULTS AND DISCUSSION

Regression models were obtained without the intercept term. This was based on the assumption that when tumbling time (X1), tumbling speed (X2), and % KCl substitution (X3) all equal zero, the product can not be prepared. The following models were selected based on the tests of hypothesis concerning the individual parameters in the second order model. The significance of each term in the model met the 20% level. However, individual terms (X1, X2, X3) were added if their interaction terms were significant at 20% level.

Textural parameters

$$\begin{aligned} \text{WBS (g)} &= 114.1 X_1 + 79.8 X_2 + 14.5 X_3 - 5.4 X_1 X_3 - 0.97 X_1 X_2 \\ R^2 &= 0.985, \text{MSE} = 62676 \text{ at } 15 \text{ df.} \end{aligned} \quad (1)$$

Where R^2 is coefficient of determination, MSE is mean sum of squares of error, and df is degree of freedom for error.

$$\text{HARD (N/cm}^2\text{)} = 5.91 X_1 + 2.44 X_2 - 0.17 X_3 - 0.14 X_1^2 - 0.003 X_3^2 - 0.22 X_1.X_2 + 0.035 X_1.X_3 \quad (2)$$

$$R^2 = 0.996, \text{ MSE} = 16.1 \text{ at } 13 \text{ df.}$$

$$\text{COH} = 0.028 X_1 + 0.012 X_2 - 0.001 X_3 - 0.001 X_1^2 - 0.001 X_1.X_2 + 7E-5 X_1.X_3 \quad (3)$$

$$R^2 = 0.997, \text{ MSE} = 2.57E-5 \text{ at } 14 \text{ df.}$$

$$\text{ELAS (cm)} = 0.066 X_1 + 0.018 X_2 + 0.003 X_3 - 0.002 X_1^2 - 3.9 E-5 X_3^2 - 0.001 X_1.X_2 \quad (4)$$

$$R^2 = 0.996, \text{ MSE} = 1.8E-3 \text{ at } 14 \text{ df.}$$

$$\text{GUM (N/cm}^2\text{)} = 1.007 X_1 + 1.024 X_2 - 0.078 X_3 - 0.001 X_3^2 - 0.089 X_1.X_2 + 0.014 X_1.X_3 \quad (5)$$

$$R^2 = 0.991, \text{ MSE} = 2.18 \text{ at } 14 \text{ df.}$$

$$\text{CHEW (N/cm)} = 0.904 X_1 + 0.484 X_2 - 0.055 X_3 - 0.024 X_1^2 - 9.94E-4 X_3^2 - 0.042 X_1.X_2 + 0.011 X_1.X_3 \quad (6)$$

$$R^2 = 0.992, \text{ MSE} = 1E-4 \text{ at } 13 \text{ df.}$$

Functional properties

$$\text{SH(5)} = 0.322 X_1 - 0.004 X_1^2 \quad (7)$$

$$R^2 = 0.862, \text{ MSE} = 1.88 \text{ at } 18 \text{ df.}$$

$$\text{CY} = 0.124 X_1 + 0.042 X_2 + 0.0004 X_3 - 0.003 X_1^2 - 0.003 X_1.X_2 \quad (8)$$

$$R^2 = 0.997, \text{ MSE} = 0.005 \text{ at } 15 \text{ df.}$$

$$\text{WHC of raw ham (5)} = 8.06 X_1 + 4.00 X_2 - 0.18 X_1^2 - 0.06 X_2^2 - 0.17 X_1.X_2 \quad (9)$$

$$R^2 = 0.998, \text{ MSE} = 21.2 \text{ at } 15 \text{ df.}$$

$$\text{WHC of cooked ham (\%)} = 3.84 X_1 + 3.90 X_2 + 0.47 X_3 - 0.05 X_2^2 - 0.16 X_1.X_2 - 0.04 X_1.X_3 \quad (10)$$

$$R^2 = 0.997, \text{ MSE} = 19.2 \text{ at } 14 \text{ df.}$$

$$\text{L (lightness)} = 5.85 X_1 + 2.90 X_2 - 0.16 X_1^2 - 0.04 X_2^2 - 0.12 X_1.X_2 \quad (11)$$

$$R^2 = 0.998, \text{ MSE} = 7.13 \text{ at } 15 \text{ df.}$$

$$\text{a (redness)} = 0.114 X_1 + 1.076 X_2 - 0.030 X_2^2 \quad (12)$$

$$R^2 = 0.990, \text{ MSE} = 1.29 \text{ at } 17 \text{ df.}$$

$$\text{b (yellowness)} = 0.797 X_1 + 0.408 X_2 - 0.004 X_3 - 0.025 X_1^2 - 0.007 X_2^2 - 0.012 X_1.X_2 \quad (13)$$

$$R^2 = 0.998, \text{ MSE} = 0.15 \text{ at } 14 \text{ df.}$$

Sensory attributes

$$\text{Colour} = 1.06 X_1 - 0.04 X_1^2 \quad (14)$$

$$R^2 = 0.990, \text{ MSE} = 0.46 \text{ at } 18 \text{ df.}$$

$$\text{Tenderness} = - 0.575 X_1 + 0.971 X_2 + 0.164 X_3 + 0.054 X_1^2 - 0.016 X_2^2 - 0.002 X_3^2 - 0.037 X_1.X_2 \quad (15)$$

$$R^2 = 0.984, \text{ MSE} = 1.57 \text{ at } 13 \text{ df.}$$

$$\text{Juiciness} = 0.65 X_1 + 0.48 X_2 - 0.04 X_1.X_2 \quad (16)$$

$$R^2 = 0.977, \text{ MSE} = 1.70 \text{ at } 17 \text{ df.}$$

$$\text{Saltiness} = 1.194 X_1 + 0.229 X_2 - 0.088 X_3 - 0.029 X_1^2 + 0.002 X_3^2 - 0.018 X_1 X_2 - 0.005 X_1 X_3 \quad (17)$$

$$R^2 = 0.995, \text{MSE} = 0.47 \text{ at } 13 \text{ df.}$$

$$\text{Off-flavour} = -0.016 X_1 + 1.366 X_2 + 0.074 X_3 - 0.039 X_2^2 - 0.003 X_3^2 \quad (18)$$

$$R^2 = 0.983, \text{MSE} = 1.88 \text{ at } 15 \text{ df.}$$

$$\text{Overall acceptability} = 2.085 X_1 - 0.069 X_3 - 0.095 X_1^2 - 0.002 X_3^2 + 0.006 X_1 X_3 \quad (19)$$

$$R^2 = 0.992, \text{MSE} = 0.67 \text{ at } 15 \text{ df.}$$

Process optimization

The above mentioned regression models provide response surfaces, and thus can be used to calculate optimum process conditions. Some of these models can be combined to form composite models. When combined, different weight can be given to the different attributes or parameters. For example, sensory attributes - (colour, tenderness, juiciness, off-flavour and overall acceptability - equal weight to each attribute. The following composite model (SENS) was obtained: (equation 20)

$$\text{SENS} = 3.2037 X_1 + 2.8126 X_2 + 0.1686 X_3 - 0.0817 X_1^2 - 0.0554 X_2^2 - 0.0066 X_3^2 - 0.0762 X_1 X_2 + 0.0059 X_1 X_3$$

The model (20) was maximized using the optimization program of Mittal and Osborne (1986). The optimum process conditions were $X_1 = 12.4 \text{ hr}$, $X_2 = 16.8 \text{ rpm}$, and $X_3 = 18.3\% \text{ KCl}$ substitution and provided $\text{SENS} = 45.1$. Similar calculations can be performed for other models.

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