Optimum Stress Relaxation Test Conditions for Beef Products

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SUMMARY: The effects of various test parameters on stress relaxation data for beef products, and the suitability of different models to describe the test data were investigated. One beef product from each of the three broad classes were laken <sup>akrent</sup> models to describe the test data were investigated. One beer product from each of the time beef). Cylindrical <sup>bken</sup> finely comminuted (frankfurter), ground beef (hamburger), and whole muscle (corned beef). Cylindrical <sup>bken</sup> finely comminuted (frankfurter) are been beef (hamburger), and whole muscle (corned beef). specimens of meat products, 10, 15 or 20 mm in diameter and 10 mm in length were prepared. These were compressed  $b_{10\%}$ , 20% or 30% of their original height for 9 min. The data was fitted in three models - Maxwell model with two elements of the stress relayation test data was normalized by elements, and Peleg (1979) and Nussinovitch et al. (1989) models. The stress relaxation test data was normalized by dividing to get modulus values. Both sample size and compression tividing the force by cross sectional sample area and strain to get modulus values. Both sample size and compression ratio (D(1) of 1.5 and any compression ratio were suitable for Table and strain to get modulus values. Doth sample area and strain to get modulus values. Doth sample area suitable for  $M_{\rm Min}$  affected model parameters. A diameter to length ratio (D/L) of 1.5 and any compression ratio were suitable for  $M_{\rm Min}$  affected model parameters. A diameter to length ratio (D/L) of 1.5 and any compression ratio were suitable for  $h_{uscle}$  foods; D/L = 1.5 and 10% or 20% compression for ground beef; and D/L = 2 and 10% or 20% compression for  $h_{uscle}$  $h_{hely}^{acle foods}$ ; D/L = 1.5 and 10% or 20% compression for gradient conditions.

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NTRODUCTION: The objectives of this study were: (i) To evaluate the effects of various test conditions on stress relaxation data for three beef products - whole muscle, ground and finely comminuted (emulsified). (ii) To evaluate the suitable. suitability of various models to describe the test results. (iii) To standardize stress relaxation test parameters for various beef products.

MATERIALS and METHODS: Particular lots of frankfurter and corned beef were supplied by a local manufacturer. The ground meat was filled in a casing in the form of a salami. This provided uniform samples, without air bubbles. The products' compositions were:

Frankfor Wa	ater	Protein	fat a	ash	
<sup>rrankfurter</sup> Ground beef Corned beef	55.9	12.6	28.5	2.9	
Corned L	54.5	15.4	26.8	3.2	
Deef	79.0	13.8	2.5	4.5	

Cylindrical specimens of the products 10 mm, 15 mm and 20 mm in diameter and 10 mm in length were prepared by <sup>An</sup> electric slicer and suitable cork borers. Stress relaxation tests were performed on an Instron universal testing height. The specimen were compressed to 10%, 20% and 30% of their original height. The specimen were compressed to 50 cm/min for the first 1 min and 2 height. The force-time curves were recorded on a chart recorder at a speed of 50 cm/min for the first 1 min and 2 cm/min c  $c_{n/min}^{sut}$ . The force-time curves were recorded on a chart recorder at a speed of 50 cm/min for the line of  $d_{ata}$  was another 8 min. Five replications were taken for each treatment. The whole experiment was run twice. The  $d_{ata}$  was  $t_{a_{1}a_{1}w_{a_{1}a_{2}w_{a_{1}a_{2}}w_$ 

MODELLING: The stress relaxation data has traditionally been described in terms of a discrete linear-Maxwell model Mohsenin, 1986):

 $F(t) = E_o + \sum_{i=1}^n E_i e^{-\frac{t}{\tau_i}}$ (1)

<sup>where</sup> F(t),  $E_0$  and  $E_i$  are the decaying parameters (modulus = stress/strain),  $\tau_i$  relaxation times and t is time.

 $e_{quation 2}$  was reported by Nussinovitch *et al.* (1989) for describing the stress relaxation data. This is a simplification of equation 1.

$$\frac{F(t)}{F_0} = A_1 + A_2 e^{-\left(\frac{t}{10}\right)} + A_3 e^{-\left(\frac{t}{100}\right)}$$
(2)

<sup>where</sup>  $F_0$  is the initial force, F(t) the decaying force, A<sub>1</sub>, A<sub>2</sub>, and A<sub>3</sub> the dimensionless constants. The unit for t is second, and 10 and 10 and 10 force, F(t) the decaying force, A<sub>1</sub>, A<sub>2</sub>, and A<sub>3</sub> the dimensionless constants. The unit for t is second,  $a_{hd}^{\text{vere } F_0}$  is the initial force, F(t) the decaying force, F<sub>1</sub>, and 10 and 100 are the fixed relaxation times in second.  $P_{eleg}$  (1979) used eqs. 3 and 4 for describing stress relaxation data:

$$Y(t) = \frac{F_0 - F(t)}{F_0}$$
(3)

$$Y(t) = \frac{a \cdot b \cdot t}{1 + b \cdot t} \tag{4}$$

where 'a' and 'b' are the constants. In the following discussion, model 1 consists of eq. 1, model 2 represents eq. 2, and the model 3 composed of eq. 2 and 4. The table is a set of the s model 3 composed of eqs. 3 and 4. The 'a' in model 3 denotes the amount of stress decay during relaxation and "the represents the 'rate' at which the attraction and "the trace of the trac represents the 'rate' at which the stress relaxes. A higher 'b' value expresses a steeper descent of the relaxation curve toward the residual value (Peleg, 1979) toward the residual value (Peleg, 1979).

In model 1, functions Fo = E0 + E1 + E3 and  $\sigma$  = E1/ $\tau$ 1 + E2/ $\tau$ 2, the derivative of the stress relaxation curve at <sup>1</sup> 0, was chosen for further statistical analysis.

The normalized experimental data was fitted in models 2 and 3 using General Linear model (GLM) procedure of the statistical Analysis System (SAS, 1989). Model 1 more fitted Statistical Analysis System (SAS, 1989). Model 1 was fitted using the method given by Mohsenin (1986) and the computer program of Rudra (1987).

I <u>Frankfurter</u> (i) <u>Model 1</u>: Table 1 shows the influence of different treatments on the model parameters. At 30<sup>th</sup> compression, no variability was noted in E1 due to complexing entry in the treatment of the compression, no variability was noted in E1 due to sample size variations. Similarly, sample size had no effect on E1 and F0 at 20% compression. No difference was noticed in E1 for the formation of the formatio and Fo at 20% compression. No difference was noticed in E0 for different sample sizes at 10% and 20% compression. Sample size has not affected  $\tau_1$  at 10% and 30% compression. Sample size has not affected  $\tau 1$  at 10% and 30% compression. However, it was higher for 30% compression compared to 10%. At 10% compression, sample size had no effect on  $\tau$ . At 10% compression, sample size had no effect on  $\tau$ . to 10%. At 10% compression, sample size had no effect on  $\sigma$ . At other compression ratios,  $\sigma$  decreased with the increase in sample diameter. (ii) Model 2: The sample size and compression ratios of decreased with the increase decreased with the increased w in sample diameter. (ii) <u>Model 2</u>: The sample size and compression ratio did not affect the parameters of model 2, this model may not be sensitive enough to provide the difference in the this model may not be sensitive enough to provide the difference in the treatments. (iii) Model 3: Only 'b' was affected significantly by treatments.

Fig.1 shows the different stress relaxation curves of different sample sizes and compression ratios. Modulus values vert higher at 30% compression than at 10% and 20%. The difference between different sample sizes was smallest at 20% compression. The recommended test conditions are: dismeter/level. compression. The recommended test conditions are: diameter/length ratio of 2 and 10% or 20% compression ratio

<u>II Ground-beef</u> (i) <u>Model 1</u>: Table 2 indicates that in general E1 increased with the increase in D/L and compression the pression that the increase in D/L and compression the pression that the increase in D/L and compression the pression that the increase in D/L and compression the pression that the increase in D/L and compression the pression that the increase in D/L and compression the pression that the increase in D/L and compression the pression that the increase in D/L and compression the pression the pression that the pression that the pression the pression the pression that the pression the pression that the pression the pression that the pression the pressionratio. Statistically, there was no effect of sample size for 10% and 30% compression. E2, Fo and  $\tau 1$  increased with the increase of  $\tau 10\%$  and  $\tau 1$  increased with the increase of  $\tau 10\%$  and  $\tau 1$  increased with the increased  $\tau 1$  i increase in sample diameter for 10% and 20% compression. E2 decreased with the increase in sample diameter on  $\tau 1$  for 30% compression. E2 decreased with the increase in sample diameter. There and  $\tau 1$  increase  $\tau 1$  for  $\tau$ was no effect of sample diameter on  $\tau 1$  for 30% compression. E2 decreased with the increase in sample diameter.  $\tau_{and}^{and}$  sample diameter, except for treatment 2. The effect was more similar sample diameter, except for treatment 2. The effect was more significant at 20% and 30% compression. E0 increased with the increase in compression ratio and  $\sigma$  decreased with the increase in compression ratio and complete the same significant at 20% and 30% compression. and  $\sigma$  decreased with the increase in compression ratio and sample diameter for 20% and 30% compression. E0 increase  $\underline{2}$ : A1, A2 and Fo were influenced by treatments. Fo increased 2: A1, A2 and Fo were influenced by treatments. Fo increased, generally, with the increase in sample diameter and

TREATMENT		E <sub>1</sub>	E <sub>2</sub>	E <sub>0</sub>	τ <sub>1</sub> , s	τ <sub>2</sub> , s	F <sub>0</sub>	σ, kPa/s	
CO	1	D/L=1	40.5	54.0	48.5	561.6	8.68	143.0	6.53
MP			a b	bc	bc	d	c	bcd	b
=10	2	D/L=	32.3	44.2	41.6	500.6	7.04	118.1	6.45
%		1.5	abc	d	cd	d	c	e	b
	3	D/L=2	22.4	56.2	48.4	758.3	9.43	127.0	5.98
	-		e	b	bc	d	c	cde	b
CO	4	D/L=1	40.0	48.4	38.2	575.4	7.36	126.6	6.86
MP			a b	bcd	d	d	c	cde	b
=20	5	D/L=	26.2	54.4	43.6	1575	14.8	127.2	3.89
%		1.5	de	bc	bcd	bc	c	de	c
	6	D/L=2	30.9	45.0	36.9	1883	24.3	112.9	2.52
			c d	c d	d	a	b	e	c d
CO	7	D/L=1	38.7	88.2	50.9	873.7	10.7	177.8	8.46
MP			abc	a	b	cd	c	a	a
=30	8	D/L=	42.8	57.2	48.1	1306	26.2	148.2	2.81
%		1.5	a	b	bc	bc	b	bc	c d
	9	D/L=2	42.8	45.7	64.7	1211	36.5	153.2	1.73
		1.5	a	cd	a	bc	a	b	d

**TABLE 1 DUNCAN'S RANKING OF MEAN VALUES OF TEST PARAMETERS FOR** 

Data with the same letter in a column are not significantly different at 95% level. D/L = sample diameter to length ratio, **COMP** = compression ratio.

TABLE 2DUNCAN'S RANKING OF MEAN VALUES OF TEST PARAMETERS OF GROUND-BEEF.THE  $E_1, E_2, E_0$  AND  $F_0$  ARE MODULUS IN kPa.

TREATMENT		E <sub>1</sub>	E <sub>2</sub>	E <sub>0</sub>	τ <sub>1</sub> , s	τ <sub>2</sub> , s	F <sub>0</sub>	σ, kPa/s	
CO MP	1	D/L=1	24.1 c	30.1 e f	46.2 b c	214.9 c	6.74 d	100.3 b c	-5.24 c d e
=10 %	2	D/L= 1.5	30.0 b c	35.9 e	44.7 b c	274.6 c	5.71 d	110.5 b	-6.56 e
	3	D/L=2	27.4 b c	69.1 b	50.3 b	1190 a b	12.0 c d	146.8 a	-6.17 d e
CO MP =20 %	4	D/L=1	24.2 c	27.8 e	28.6 e	383.9 c	7.1 d	80.6 c	-4.15 b c
	5	D/L= 1.5	32.8 b c	47.8 d	34.5 d e	927 b	11.6 c d	115.1 b	-5.07 c d
	6	D/L=2	46.6 a	50.3 d	58.9 a	1364 a	45 b	155.8 a	-1.29 a
CO MP =30 %	7	D/L=1	40.0 a b	84.0 a	38.2 c d	1213 a b	17.4 c d	162.2 a	-6.08 d e
	8	D/L= 1.5	50.0 a	59.5 c	42.4 b c d	1191 a b	24.7 c	152.0 a	-3.11 b
	9	D/L=2	50.3 a	49.1 d	64.2 a	1442 a	66.4 a	164.6 a	-1.10 a

Data with the same letter in a column are not significantly different at 95% level. D/L = sample diameter to length ratio. COMP: compression ratio.

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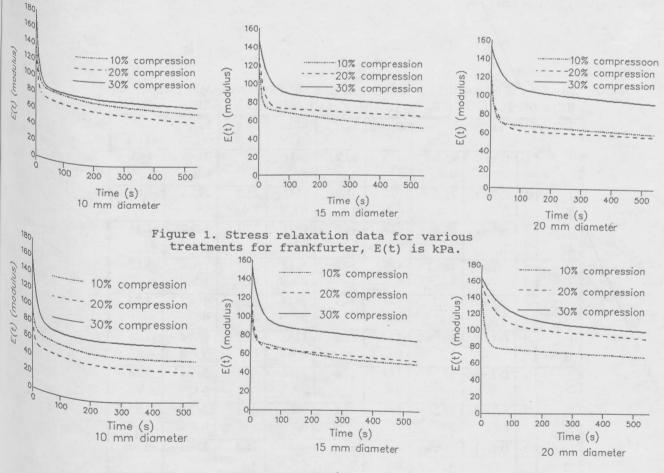
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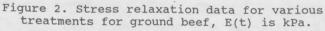
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compression ratio. (iii) Model 3: Treatment affected 'a' and 'Fo'. Fo increased with the increase in compression ratio and sample diameter. and sample diameter.

Fig.2 shows the stress relaxation curves for different treatments. The recommended test conditions are:  $D/L = 1.5 an^{th}$ 10% or 20% compression ratio. It is important to provide the sample size and compression ratio when providing the information on stress relaxation test parameters. It is used to be a size and compression ratio when providing the sample size and compression ratio when providing the same sintervide the same size information on stress relaxation test parameters. It is difficult to compare these parameters collected at various test

III <u>Whole muscle (corned beef)</u> (i) <u>Model 1</u>: Table 3 indicates that sample size has not influenced E1 for 10% and 20% compression. However, E1 and E2 increased with the increased compression. However, E1 and E2 increased with the increase in sample diameter for 30% compression.  $\tau 1$  increased with the increase in sample diameter for 30% compression.  $\tau 1$  increased with the increase in sample diameter for 10% compression. with the increase in sample diameter for 10% compression. In general,  $\tau^2$  increased with the increase in test conditions except for treatment 8. E0 increased with the increase in rest conditions and with the increase in test conditions. except for treatment 8. E0 increased with the increase in sample diameter for 10% compression. E0 also increased with the increase in sample diameter for 10% compression. E0 also increased with the increase in compression and from 20% to 30%. For large parts of 0.00% to 0.00% for large parts of 0.00% to 0.00%. the increase in compression ratio from 20% to 30%. For larger sample (D/L = 2), F0 increased with the increase of compression ratio.  $\sigma$  decreased with the increase in sample diameter for 10% compression. E0 also increased with the increase of  $\sigma$  and  $\sigma$  and  $\sigma$  are the increase of t compression ratio.  $\sigma$  decreased with the increase in sample diameter for all compression ratios. (ii) Model 2: Only and Fo were affected by treatments. Increase in sample size increased 4.1.6.20% and Fo were affected by treatments. Increase in sample diameter for all compression ratios. (ii) Model 2: Only with the increase in sample diameter from 15 mm to 20 mm (iii) Model 20% and 30% compression. Fo increase by with the increase in sample diameter from 15 mm to 20 mm. (iii) Model 3: Only 'a' and Fo were influenced by treatments.

Fig. 3 shows the stress relaxation curves for various treatments. The recommended test conditions are:  $D/L = 1.5 a^{\mu}$ compression ratio from 10% to 30%.

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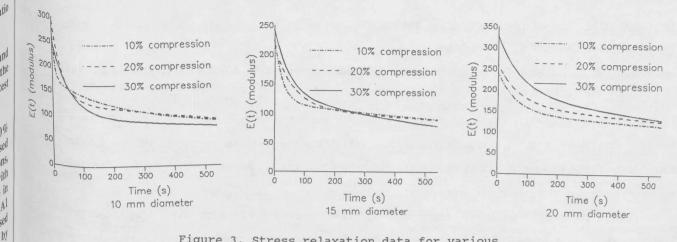
### **TABLE 3**

## DUNCAN'S RANKING OF MEAN VALUES OF TEST PARAMETERS OF A BEEF MUSCLE, THE E., E., E. AND F. ARE MODULUS IN kPa.

TREATMENT		E <sub>1</sub>	E <sub>2</sub>	E <sub>0</sub>	τ <sub>1</sub> , s	τ <sub>2</sub> , s	<b>F</b> <sub>0</sub>	σ, kPa/s	
	1	D/L=1	93.5 b	89.9 d	80.2 a	261 e	7.9 d	272.6 c b	-14.1 d
CO MP =10 %	2	D/L=1. 5	75.9 b c	107 c d	41.9 c d	1216 b c d	25.8 c d	225.2 c d	-7.40 c
	3	D/L=2	99.4 b	94.4 d	46.5 b c d	1591 a b	59.1 a	240.2 b c d	-2.35 a
СО	4	D/L=1	103.7 b	156 a	30.6 d	1123 b c d	32.2 b c	290.6 a b	-6.53 b c
	5	D/L=1. 5	76.3 b c	101 c d	33.1 d	1833 a	62.5 a	210.3 d	-2.26 a
MP =20 %	6	D/L=2	107.8 b	93.3 d	57.3 b c	1288 a b c	67.7 a	258.4 b c d	-1.71 a
	7	D/L=1	62.1 c	148 a b	37.8 d	1466 a b	59.1 a	247.7 b c d	-3.24 a b
CO MP	8	D/L=1. 5	96.3 b	109 c d	37.0 d	658 d e	48.1 a b	242.3 b c d	-2.83 a
=30 %	9	D/L=2	138.5 a	129 b c	61.0 b	808 c d e	71.4 a	328.5 a	-2.14 a

Data with the same letter in a column are not significantly different at 95% level. D/L = sample diameter to length ratio. **COMP:** compression ratio.

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Figure 3. Stress relaxation data for various treatments for beef muscle, E(t) is kPa.